ECONOMIC AND EFFICIENT METHOD OF DESIGN OF A FLUMED CANAL FALL

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ABSTRACT

Innumerable falls are to be provided in irrigation canals where ground slope exceeds the permissible bed slope of a canal. In the conventional method of design, fluming ratio is fixed arbitrarily irrespective of inflow Froude's number. Long length of inlet and outlet transitions are provided to prevent flow separation. Transition and dissipation structures are separate resulting in high costs. Hydraulic performance of the conventional fall structure is also not so satisfactory . Analytical and experimental studies were conducted by the author to find an efficient and economic method of design of falls. Optimum fluming ratio and optimum length of transitions are found both for economy as well as efficiency. An efficient and economic stilling basin , with rapidly diverging side walls and adversely sloping floor, which act simultaneously for energy dissipater and transition, has been recommended. An example has been worked out to illustrate the design procedure of a typical canal fall.

Keywords: Canal fall, Fluming ratio , Transition, Energy Dissipation, Hydraulic Efficiency

1.0 INTRODUCTION

Canal falls are needed for negotiating steep terrain slope. Falls are used as control structures to regulate flow depth, maintain depth- discharge relation, flow diversion, flow measurement etc. They are often combined with local communication bridges and cross regulators. In unlined canals where canal width is large, they are usually flumed to reduce cost. In all such flumed canal falls, a pair of transitions are to be provided both upstream (Contracting Transition) and downstream (Expanding Transition) of the flumed section for smooth flow at entry and exit of fall. They are to be invariably provided with energy dissipaters to avoid erosion downstream. In the conventional design of a fall, it is customary to flume the canal by restricting the normal waterway. Extent of fluming will be governed by Froude's number of incoming flow (F_1) and the desired value of Froude's number of flow in the flumed section(F_0) (Mazumder,1978 **).** Any fluming beyond a critical limit (known also as choking limit when $F_0 = 1$) will cause excessive afflux resulting in a long backwater reach when the canal regime and proportional flow condition i.e the normal depth-discharge relation (Mazumder & DebRoy,1999) is lost. Cost of connecting the flumed section with the normal canal section by providing classical transition structures is excessively high. The demerits of conventional design of energy dissipaters, inlet and outlet transitions with long length and complicated shapes have been discussed elsewhere (Mazumder,1967). In this paper, author has suggested an innovative, economic and hydraulically efficient design of fall by employing recent advances in hydraulics.

2.0 DEVELOPMENT IN FALL DESIGN

Depending upon discharge and height of fall, different design of falls have been evolved over time e.g.(i)Montagu type (ii) Ogee type (iii)Stepped type (iv) Trapezoidal notch type (v) Vertical drop type (vi)Inglis type (vii) Sarda type (viii) Straight glacis type (ix) Pipe type (x)Syphon type (xi) Well type etc. Detailed design procedure of these falls are available in standard text books (Arora, 1996, Aswa, 1993,Mazumder,2007). Most of these designs have been developed by project authorities based on the local requirement and knowledge available at the time. The design proposed in this paper is based on the recent development in hydraulics and the laboratory experiments carried out by the author and the young students working with him with a view to economise the cost and at the same time making the design hydraulically more efficient.

3.0 IMPROVED DSIGN OF FLUMED CANAL FALL

As already mentioned, in unlined canals where the mean velocity of flow has to be restricted to avoid erosion, falls are invariably flumed for economy. In the conventional design, flume extends up to the stilling basin end followed by expanding transition. This makes the fall very costly since the entire length from entry of contracting transition to the exit of expanding transition must be paved and the pavement has to be designed to resist uplift pressure. In the proposed design, the stilling basin is provided with expanding side-walls right from the toe of downstream glacis (Fig.1) so that no separate expanding transition is needed resulting in considerable reduction in the length of paved floor and cost of fall .

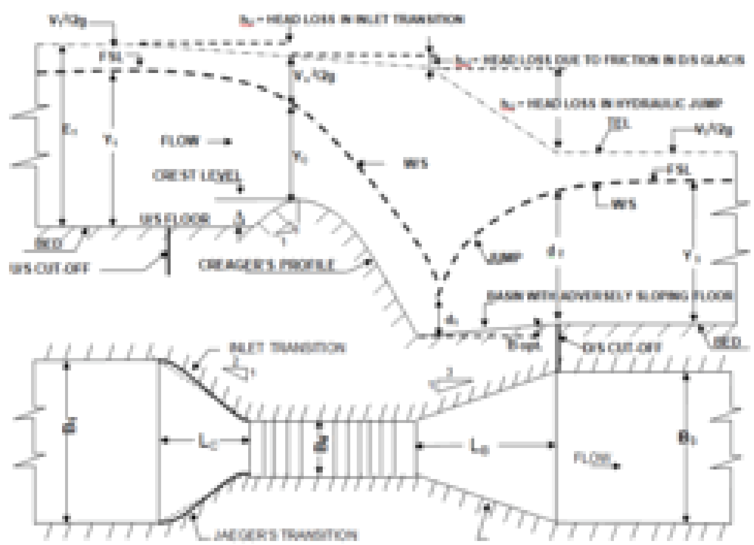


Fig.1 Plan and Section of Proposed Fall (See Appendix-1)

3.1 Hydraulic Aspects of Design

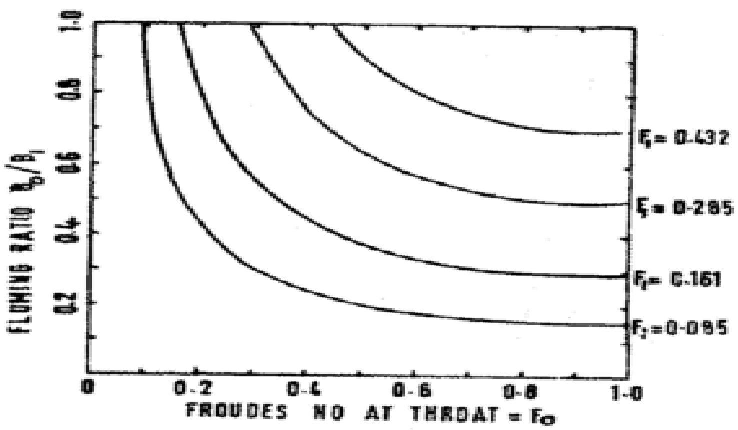
In this section, the different hydraulic aspects of the proposed design in regard to fluming, flow regime, transition and energy dissipation are discussed briefly with a worked out example at the end (Appendix-1) to help the designers.

3.1.1 Hydraulics of Flume

If B_1 and B_0 are the mean widths of flow at the normal and flumed sections of a canal fall respectively (Fig.1), it can be proved that the fluming ratio (B_0/B_1) may be expressed as

$$B_o/B_1 = (F_1 / F_o) \left[(2+F^2_o) / (2+F_1^2)\right]^{3/2} \qquad (1)$$

Where, F_1 and F_0 are the Froude's number of flow at the normal and flumed sections respectively. Fig.2 shows the functional relation between B_0/B_1 and F_0 given by equation(1)for different values of F_1 for approaching flow. It may be seen that higher the F_1-value, less is the opportunity of fluming to avoid flow choking. F_1 - values indicated in the figure were found corresponding to mean width of flow (B_1) for four different canals with varying bed slope and discharge. There is hardly any advantage /economy if fluming is made such that F_0 exceeds approximately 0.70. Also, flow surface becomes wavy when F_0 >0.70, with highest degree of wave amplitude at critical flow at $F_0 = 1$. Excessive fluming also causes high loss in head due to high velocity of flow at the flumed section resulting in large afflux.



6Fig.2 Showing Interrelation between F_1, F_0, and B_0 / B_1

3.1.2 Optimum Flume Width (B_0) and Crest Height(Δ) to Maintain Depth- Discharge Relation

Canal falls are control structures which can be used also for measuring flow through the canal. In case the fluming is too high, crest height above the canal bed, Δ (shown in Fig.1) will be low. On the other hand, if fluming is too low, the crest height will be more. An optimum width of throat (B_0) and corresponding crest height (Δ) were determined theoretically (Mazumder, S.K. & Debroy Indraneil, 1999) such that the proportionality of flow with negligible afflux will occur. Equations 2 gives the optimum width at throat (B_0) and equation 3 gives the corresponding crest height (Δ) for maintaining proportionality of flow for all discharges passing through the canal.

$$B_0 = [0.7\,(Q_{max}^2 - Q_{min}^2) / (E_{1max} - E_{1min})]^{3/2} \qquad (2)$$

$$\Delta = E_{1max} - 3/2\,[(Q_{max} / B_0)^2 / g]^{1/3} \qquad (3)$$

where Q_{max} and Q_{min} are the maximum and minimum flow through the canal ; E_{1max} and E_{1min} are the corresponding maximum and minimum specific energy of flow given by

$$E_{1max} = Y_{1max} + V_{1max}^2/2g \text{ and } E_{1min} = Y_1 min + V_{1min}^2/2g \qquad (4)$$

Here, Y_{1max} and Y_{1min} are the normal flow depths and V_{1max} and V_{1min} are the mean velocities of flow in the canal upstream of the drop corresponding to Q_{max} and Q_{min} respectively. The various symbols used in the equations, the flumed fall, the inlet and outlet transition structures etc. are illustrated in Fig.1. An illustrative example has been carried out in appendix-1.

3.1.3 Ogee Type Glacis to Prevent Flow Separation

Ogee type profile (USBR ,1968) may be adopted for the downstream glacis to ensure smooth flow over the glacis free from any separation. Co-ordinates of Ogee profile can be obtained from equation(5) with crest as origin.

$$Y/H_0 = K\,(X/H_0)^{n} \tag{5}$$

where X and Y are the co-ordinates at any point on the profile, H_0 is the energy head above crest, K and n are coefficients governed by approach velocity head and shape of upstream geometry of the profile. K and n - values can be obtained from the text book,"Design of Small Dams" .

4.0 DESIGN OF CONTRACTING AND EXPANDING TRANSITIONS

As stated earlier these transitions are to be provided for smooth flow at entry and exit of flumed fall.

4.1 Contracting Transition

As shown in Fig.1, contracting transition connect the normal section with the flumed section. In a contracting transition, potential energy is converted to kinetic energy of flow. Afflux upstream of a fall is governed by the head loss in the transition. More is the head loss, more will be the afflux. Relation between head loss and efficiency (η_i) in a contracting transition can be expressed as

$$\eta_i = 1 / (1+C_i) \tag{6}$$

where C_i is inlet head loss coefficient given by the relation

$$C_i = h_{Li} / [\,(V_c^2 - V_1^2)/2g\,] \tag{7}$$

where h_{Li} is the loss in head in the inlet transition, V_c and V_1 are the mean velocities of flow at crest and at normal sections of the canal upstream of the fall respectively.

Different shapes of contracting and expanding transitions have been proposed by several research workers from time to time (Hinds-1928 , Mitra-1940 , Chaturvedi-1963 , Mazumder-1977, Vittal et al-1983, Garde and Nasta-1990, Swamee et al-1992). Shape of Jaeger (1956) type transitions is defined by equations 8 to 12 given below. Fig.3 shows the hydraulic efficiency (η_i) of Jaeger type contracting transition having different axial lengths governed by average rate of flaring varying from 0:1 to 5:1 (Mazumder et al,1978)

$$V_x = V_1 + a\,(1 - \cos\Phi) \tag{8}$$

$$\Phi = \pi x / L_c \tag{9}$$

$$y_x = y_1 - a/g\,[(a+V_1)(1-\cos\Phi) - 1/2\,a\,\sin^2\Phi] \tag{10}$$

$$a = ½\,(V_0 - V_1) \tag{11}$$

$$V_x B_x y_x = Q = V_1 B_1 y_1 \tag{12}$$

where V_x, y_x and B_x are the mean velocity, flow depth and mean flow width at any distance 'x' from the end of inlet transition (i.e. throat section) respectively, L_c is the axial length of inlet contracting transition. and V_0 is the mean flow velocity at throat/flumed section at the exit of inlet transition. Width of flow section (B_x) at any axial distance 'X' from exit end of inlet transition can be found from the continuity equation (12). An example has been worked out to illustrates the design procedure (Appendix-1).

4.2 Expanding Transition

A pair of symmetric expanding transition is to be provided for connecting the flumed section with the normal canal section as illustrated in Fig.1. In the conventional design, expanding transition starts from the end of classical stilling basin and ends in the normal canal section. This is necessary since the sub-critical mean velocity of flow [$V_2 = Q/(Bo*d_2)$] at the exit end of flumed basin (of width, B_0) is substantially higher than the normal mean velocity (V_3) in the canal. Main function of the expanding transition is to diffuse the sub-critical flow from V_2 to V_3 so that there is no scour in the tail channel downstream of the fall. Since the sub-critical flow in an expanding transition is subjected to an adverse or positive pressure gradient, the flow separates if the axial length of transition is insufficient. It has been established (Kline & Cochran -1958 , Gibson-1910) that if the total angle of expansion exceeds about 10^0 to 12^0, flow will separate from the boundary resulting in poor efficiency ($\eta_0 = 1-C_0$) and non-uniform distribution of velocity at the exit end of expansion. Mazumder (1977) tested eddy shaped (Ishbash &Lebedev,1967) expanding transition of different lengths and found that for maximum hydraulic efficiency, the axial length of transition must be about 7 to 8 times the offset [$1/2(B_3 - B_0)$] in order to ensure separation- free uniform flow at the end of transition. Fig.3 shows the variation of efficiencies in contracting and expanding transitions with different axial lengths governed by average side splay.

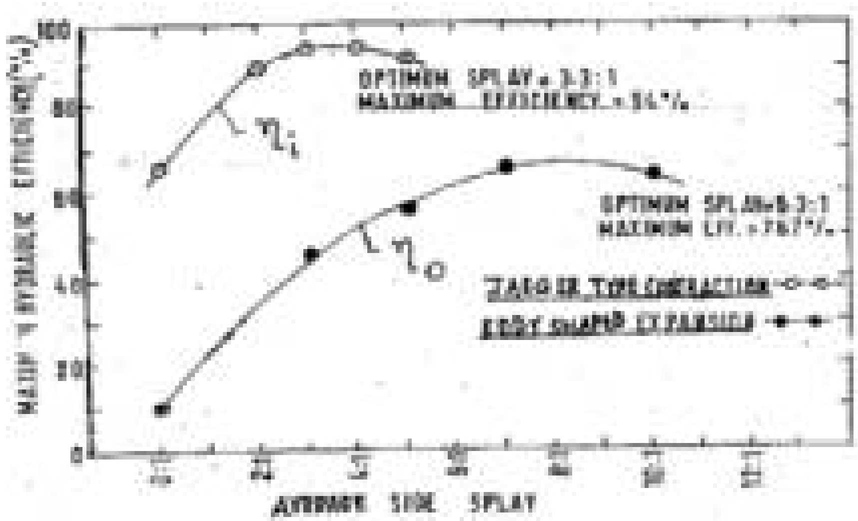


Fig.3 Variation of Efficiency in Contracting and Expanding Transition with Length

5.0 DESIGN OF STILLING BASIN

Stilling basin is provided to dissipate the kinetic energy of flow within the stilling basin. In a classical basin, width of the basin is kept the same as the width of flumed fall (B_0) up to the end of the basin, length of which is usually fixed by the length of a classical hydraulic jump in the rectangular basin. The basin length varies from 4 to 6 time the conjugate depth (d_2)depending on type of stilling basin determined by F_{t1} and Ut_1-values. where U_{t1} and $F_{t1}$are the velocity and Froude's number of flow at the toe of downstream glacis respectively. Further details of design of classical hydraulic jump type stilling basins are given in several text books on hydraulics. (Chow-1973 , Ranga Raju-1993 , USBR-1968 , Hager-1992).

The cost of stilling basin followed by a classical expanding transition in the conventional design of a canal fall, as indicated by dotted line (in plan) in Fig.4, is exorbitantly high. By using different types of appurtenances (like vanes, bed deflector, basin blocks etc) for preventing flow separation, Mazumder and Naresh(1988) developed a stilling basin with rapidly diverging straight side walls having axial length equal to three times the offset i.e.3(B-b) as shown in Fig.4. The basin functions both as energy dissipater and flow diffuser simultaneously. Without appurtenances, there will be violent separation of flow and highly non-uniform flow at the exit end of the basin. With appurtenances, there is high hydraulic efficiency and the flow becomes highly uniform at the exit.

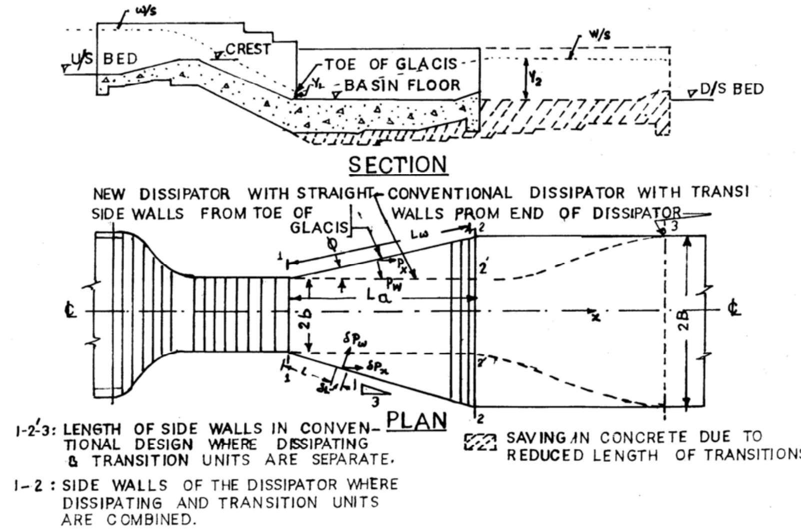


Fig.4 Plan & Sectional View of a Canal Fall Showing Proposed Design (Full Line) and the Conventional Design (in Dotted line)

To reduce the additional cost of appurtenances, Mazumder (1987a,1987b,1994) developed an innovative method of boundary layer flow control by providing adversely sloping basin floor. Optimum value of inclination of basin floor (β_{opt}) corresponding to a given angle of divergence of the side wall (Φ), as indicated in Fig-5, can be expressed as

$$\beta_{opt} = \tan^{-1}[\,(d_1^2+d_2^2 +d_1\, d_2) \tan\Phi \,/\, (b\, d_2 +Bd_1 +2bd_1 + 2Bd_2)]$$

$$= \tan^{-1}\,[2\,(y_1/b) \tan\Phi\, (1+\alpha + \alpha^2\,) \,/\, (2 + 2\,\alpha\, r + \alpha + r\,)\,] \qquad (13)$$

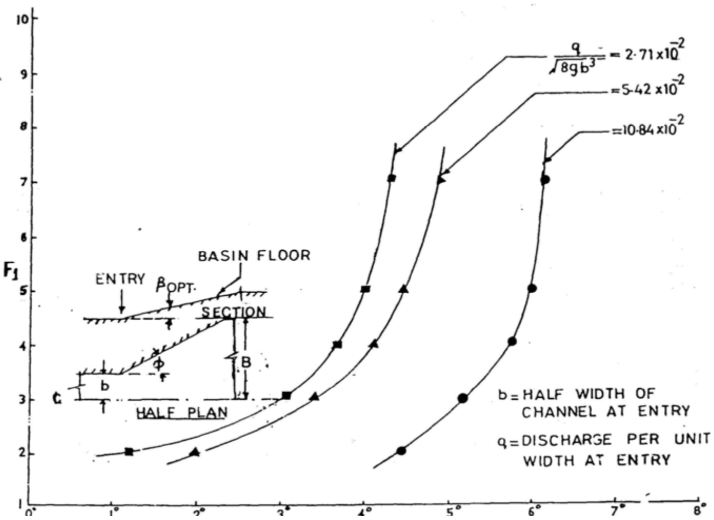
where, $\alpha = d_2 / d_1$, $r = B / b$, d_1 and d_2 are the pre-jump and post- jump depths, b and B are the half widths of the basin at the entry and exit respectively. The conjugate depth ratio, α, in this non prismatic stilling basin with adverse bed slope such that the wall reaction is balanced by bed reaction can be expressed by the relation

$$F_1^2 = 1/2\, [(1 - \alpha^2\, r) \,/\, (1 - \alpha\, r)\,]\, \alpha\, r \qquad (14)$$

In a prismatic channel of rectangular section when r =1 (i.e b=B), equation (14) reduces to the conjugate depth relation in a classical hydraulic jump given by

$$\alpha = d_2/d_1 = !/2\, [(8F_1^2 +1)^{1/2} -1] \qquad (15)$$

Experimental values of β_{opt} for best performance of the basin with 3:1 flaring of side walls are given in Fig.5. Method of computing the theoretical and experimental values of β_{opt} has been explained through an illustrative example given in appendix-1.



β opt

Fig.5 Optimum Inclination of Basin Floor(β $_{opt}$.) for Different Values of Pre-jump Froude's No. F_1

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Apendix-1
ILLUSTRATIVE EXAMPLE

Design a a canal fall with data given below:
Full supply Discharge in the canal, Q_{max} = 99.1 cumec
Full supply depth, Y_{1max} = 3.629 m
Mean Flow width of canal at FSL =29.87m
Longitudinal slope of bed = 1 in 8,000
Manning's roughness coefficient, N =0.025
Height of fall =3m
Minimum flow in the canal Q_{min} =21.5 cumec
Corresponding minimum depth of flow =Y_{1min}= 1.38 m

Computation of Flume width at throat (Bo) and Crest height (Δ)
From Proportionate Flow/ Flow Regime Consideration
V_{1max} = 0.914 m/s, $E_{1max} = Y_{1max} +(V_{1max})^2/2g$ = 3.672 m, $F_1= V_{1max}/(g\ Y_{1max})^{1/2}$ =0.153
V_{1min} = 0.522 m/s, $E_{1min} = Y_{1min} + (V_{1min})^2 /2g$ = 1.394 m
$B_0 = [\ 0.7\ (Q_{max}^{2/3} - Q_{max}^{2/3}) / (E_{1max} - E_{1min})\ ]^{3/2}$ = 8.64 m, Y_0 =Yc =2.374 m and F_0 =1.0
Since the flow at critical stage is wavy in the flumed section and from Fig.1, it is noticed that for an approaching flow Froude's number, F_1 = 0.153, there is hardly any economy in fluming beyond
F_0 =0.6, adopt F_0 = 0.6 for determining economic fluming ratio given by equation (1) i.e.
$B_o/B_1 = (F_1/F_o)\ [\ (2+F^2_o) / (2+F_1^2)]^{3/2}$ = 0.322 and hence B_0 = 8.9m;
Adopted bed width at flumed section, B_0 = 10m
Corresponding value of crest height, $\Delta = E_{1max} - 3/2\ [(Q_{max}^2 / B_0^2)/g]^{1/3}$ = 0.44m
Assuming no loss in head in inlet transition i.e. Ci = 0 or h_{Li} = 0, $E_0 = E_1$
or, $E_0 = Y_0 + Vo^2/2g$ = 3.672 and $q_0 = Q/B_0 = 9.9 = V_0\ Y_0$
Solving by trial, Y_0 = 3.176 m and V_0 = 3.118 m/s; $F_0 = V_0 / (gY_0)^{1/2}$ = 0.558
Check: $B_o/B_1 = (0.153/0.558)\ [(2+0.558^2)/ (2 + 0.153^2)]^{3/2}$ = 0.335 and B_0 = 0.335* 29.87= 10m

Design of Contractingt Transition

With 2 : 1 average side splay, axial length of inlet transition, Lc = ½ $(B_1 - B_0)$*2 = 19.87 say 20m
Adopt Jaeger type transition given by Equations (7) to (11) as follows:
$a = 0.5\ (V_o - V_1) = 0.5\ (3.118 - 0.914) = 1.102$, $\Phi = \pi x / L_c = \pi x / 20$
$V_x = V_1 + a\ (1 - \cos\Phi) = 0.91 + 1.102(1 - \cos\Phi)$
$Y_x = Y_1 - a/g\ [(a+V_1)\ (1-\cos\Phi) - 1/2\ a \sin^2\Phi] = 3.629 - [0.227(1-\cos\Phi) - .062 \sin^2\Phi]$

X (m) =	0	5	10	15	20
Φ_x(degree) =	0	45	90	135	180
V_x(m/s) =	0.914	1.234	2.016	2.795	3.118
Y_x(m) =	3.629	3.499	3.404	3.272	3.176
B_x(m) =	29.87	22.90	14.19	10.83	10
F_x =	0.153	0.211	0.346	0.493	0.558

Jaeger Type Inlet transition curve is obtained by plotting widths B_x at different X-values as shown in Fig.1.

Design of Ogee-type Glacis

Assuming that there is no regulator over crest, the co-ordinates of the curved d/s glacis are found from Creager's formula (Eq.5), with $H_0 = E_1 - \Delta$ =3.232

$$Y/H_0 = K\,(X/H_0)^{n}$$

K and n values are found to be 0.56 and 1.75 for approach velocity head ($h_a = V_1^2/2g$) of 0.043 m and design head above crest (H_0 = of 3.232m (3.672- 0.44) respectively from USBR[6].publication 'Small dams'.

X(m) =	0.25	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	4.663
X/H_0 =	0.078	0.155	0.309	0.464	619	0.774	0.928	1.083	1.237	1.392	1.442
Y/H_0 =	0.006	0.021	0.073	0.146	0.242	0.357	0.491	0.643	0.812	0.999	1.064
Y(m) =	0.019	0.068	0.236	0.472	0.782	1.153	1.567	2.078	2.624	3.220	3.440

The X,Y co-ordinates are plotted with crest as origin to obtain the d/s glacis profile as shown in Fig.1.

DESIGN OF STILLING BASIN WITH DIVERGING SIDE WALLS

Assuming no head loss up to toe of the d/s glacis, specific energy of flow at toe (E_t) is given by

$E_{t1} = E_{1max}$ + height of drop = 3.672 +3 = 6.672 = $d_1 + U_t^2/2g$

$q = Q/B0 = 9.9 = d_1 * U_t$

where d_1 and U_1 are the pre-jump depth and velocity of flow at toe of d/s glacis respectively. Solving the above two expressions by trial

d_1 =0.84 m and U_1 = 10.72 and F_{t1} = =3.73

Axial Length of the Basin: $L_b = 3\,(B_1 - B_0)/2$ = 29.8m say 30m

Conjugate depth ratio for the non-prismatic basin is given by equation (15)

$$F_1^2 = 1/2\,[(1-\alpha^2 r)/(1-\alpha r)]\,\alpha r$$

Putting $F_1 = F_{t1}$ = 3.73, r =B/b (Fig.5) = 2.987, the above eqation reduces to

$$\alpha^3 - 9.95\,\alpha + 3.219 = 0$$

Solving by trial, α =3 and $d_2 = 3d_1 = 3(0.84)$ =2.52m and submergence =3.629/2.52 =1.44 i.e.the basin will operate under 44% submergence at maximum flow which is permitted as per test results.

Theoretical value of basin floor inclination , β_{opt} is given by equation 14

$$\beta_{opt} = \tan^{-1}\,[2\,y_1/b\,\tan\Phi\,(1+\alpha+\alpha^2)\,/\,(2+2\,\alpha\,r+\alpha+r)\,]$$

With $y_1 = d_1$ =0.84m, b = 5m, $\tan\Phi$ = 1/3 and r = 2.987, $\beta_{opt} = 3.36^0$

Experimental value of β_{opt} can be found from Fig.5 as follows:

$$q\,/\,(8gb^3)^{1/2} = 9\,/\,(8*9.8*5^3)^{1/2} = 0.091 = 9.1*10^{-2}$$

corresponding to above value of $q/(8gb^3)^{½}$ and F_1 =3.73. $\beta_{opt} = 4.5^0$ (from Fig.6)

Provide basin Floor slope of $\beta_{opt} = 4.5^0$ for best performance.

Fig.1 is drawn on the basis of above mentioned computations.